CFD ANALYSIS OF BACK PRESSURE OF REACTIVE MUFFLER

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ABSTRACT
The present study describes the analysis of back pressure of the muffler by using CFD simulation. The CFD analysis is done to avoid the tedious experimentation. The flow simulation is carried out using k-ε turbulent model as it is most suitable for turbulent flows having less converging time. Total four cases were analyzed including the base model muffler. Thus three modifications were done in muffler geometry. The modification with reduced baffle spacing produced least back pressure with reduction in back pressure by 9.60%.

INTRODUCTION
Engine exhaust is traditionally carried through muffler. They are used to reduce the intensity of noise generated by the combustion process from an internal combustion engine. The word muffler is very similar to a silencer. A silencer has been the traditional name for noise attenuation devices, while a muffler is smaller, mass-produced device designed to reduce engine exhaust noise. The main function of a muffler is to reduce the noise emitted by the engine.

1.1 REACTIVE MUFFLER:
In this type of muffler Inlet and outlet tube are extended in chambers as shown in fig 1.1. These mufflers generally consist of several pipe segments that interconnect with a number of larger chambers. These are most widely used to attenuate the exhaust noise of internal combustion engines.

1.2 BACK PRESSURE
Back pressure is defined as the extra static pressure exerted by muffler on engine through restriction in flow of exhaust gases. Higher Back pressure can cause decrease in engine efficiency or increase in fuel consumption, overheating, and may result in a complete shutdown of engine.

Many researchers have worked in the field of acoustics and back pressure in order to increase the transmission loss of the muffler as their prime objective and to reduce the back pressure as the secondary. Some of them have also tried to develop an empirical relation between the transmission loss and the muffler dimensions. Some of the reputed journal papers describing the findings of the authors are discussed below:

P. S. Yadav et al.[1] studied the optimization of silencer as an integrated approach i.e., for transmission loss and backpressure. They developed an integrated methodology to predict the performance of the silencer at the design stage resulting in an optimized time and cost effective design. The acoustical and engine performance of silencer was predicted using FEM/BEM and CFD techniques. Parametric studies were carried out to find the effect of geometry on the transmission loss and backpressure. Transmission loss of
various configurations was evaluated using a 1D simulation code GT-Power. A steady state analysis was carried out using 3D CFD code FLUENT to predict the backpressure for various silencer configurations. They achieved the optimized design using integrated methodology, which met the acoustic as well as backpressure target requirements. They benchmarked a methodology for the optimized design of silencer, which takes into account the noise as well as the back pressure constraints and finds the performance parameters like TL and backpressure, which form the basis for the design of silencer.

Jianhua Fang et al. [2] studied the Pressure Loss for a Muffler Based on CFD and experimented on it. They simulated the flow field of a muffler based on CFD technique at a certain engine velocity and analyzed the pressure distribution internal the muffler. They found that with increased engine velocity, the pressure drop across the muffler became higher. For the same engine velocity with lower punching rate, the pressure loss increased.

Shital Shah et al. [3] developed a practical approach to design, develop and test muffler particularly reactive muffler for exhaust system, which gave advantages over the conventional method with shortened product development cycle time and validation. They emphasized the importance of the design methodology as a practical approach from the concept design to proto manufacturing and validation of exhaust muffler.

Wang Jie et al. [4] created a three-dimensional solid model of muffler by ProE and analyzed by ANSYS. The method of data transformation between ProE and ANSYS was prepared. Muffler natural frequencies and modal shapes were calculated by the FEM analysis software named ANSYS, by which modal shapes are displayed in the form of animation.

N. V. Pujari et al. [5] developed an integrated methodology using CFD technique to predict the acoustical and engine performance of the muffler. This research work resulted in the best optimized design achieved using integrated methodology, which meets the acoustic as well as backpressure target requirements. This study presents a benchmark methodology for the optimized design of silencer, which takes into account the noise as well as the backpressure constraints and finds the performance parameters like Acoustic performance (db) and backpressure, which form the basis for the design of silencer. The methodology developed is helpful for the manufacturers as well OEMs to reduce the design cycle time for silencer.

From the literature review and all the other aspects, some highlights of finding are below:

1. If the diameter of the perforation is increased the backpressure decreases sharply. The change in diameter of perforations has remarkable effect.
2. Design methodology emphasis on modern CAE tools for optimization of overall system design to choose the best concept.
3. The Backpressure reduced almost by 75% if the porosity is doubled. Also, if the diameter of the perforation increases the backpressure decreases sharply. The change in diameter of perforations has remarkable effect on back pressure.
4. The CFD simulation software can be used in designing and simulations. The simulations give valuable information regarding the velocity field, pressure field, density field and temperature field of the exhaust muffler. This is important because save time and many in the production process through the identification of eventual problems before the exhaust muffler is build. The effect of baffle spacing on back pressure needs to be studied in detail.

So in this work, the effect of baffle spacing on back pressure is studied along with effect of change in perforation size on the value of back pressure.

**CFD SIMULATION**

The simulation of the CAD models is carried out in software package STAR CCM+. Muffler has a complex geometry structure. The Fig.3.1 shows the insight of muffler structure. In the given muffler model, two baffle plates, one inlet and one outlet pipe are used. The inlet pipe is bent at 90° on which the perforations are made. The outlet pipe is straight one having two baffle plates. One of the baffle plate on the outlet pipe is having perforations of 3 mm diameter. Other baffle is without any perforations. The geometry is modelled in PRO ENGINEER 5.0 software.
2.1 COMPUTATIONAL MESH:
The CAD Model in Para solid format was imported in STAR CCM+. Then geometry clean-up was done and the surface mesh was created using triangular elements. For the gas volume, unstructured mesh has to be created. The Fig. 3.2 shows the meshed model

2.2 BOUNDARY CONDITIONS:
The Table 3.1 shows boundary conditions used for simulations. For simulation, velocity inlet condition and pressure outlet condition were used for inlet and outlet respectively.

<table>
<thead>
<tr>
<th>Parameters</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>Inlet Condition</td>
<td>Velocity Inlet</td>
</tr>
<tr>
<td>Inlet Velocity</td>
<td>20, 40, 60, 80 m/s</td>
</tr>
<tr>
<td>Outlet Condition</td>
<td>Pressure Outlet</td>
</tr>
<tr>
<td>Turbulent Model</td>
<td>Standard k-ε turbulent model with standard wall functions</td>
</tr>
<tr>
<td>Wall Surface Specification</td>
<td>Smooth, No-slip wall</td>
</tr>
</tbody>
</table>

SIMULATION RESULTS AND DISCUSSION:
The results of simulation of different muffler configurations are discussed below.

3.1 CASE-1 SIMULATION:
The simulation results for base model muffler are shown in fig. 3.1. The velocity near inlet pipe walls (after bent section) was higher. The velocity near outlet was found higher. It was observed that the pressure changes among the expansion chambers. The pressure in inlet pipe at bent section was observed higher. The back pressure observed was around 4196 Pa.
3.2 CASE-2 SIMULATION:
The Fig. 3.2 (a and b) shows the velocity and pressure distribution for modified perforation diameter of 4 mm. The simulation back pressure observed was around 4343 Pa. Thus the back pressure increases in this modification.

3.3 CASE-3 SIMULATION:
The Fig. 3.3 above shows the velocity and pressure distribution for perforation size of 4 mm and baffle spacing 165 mm. The back pressure observed was around 4240 Pa. This is lower than the corresponding back pressure for the Case-2 muffler.
3.4 CASE-4 SIMULATION:

Fig. 3.4 shows the pressure and velocity distribution for the muffler with perforation size of 3 mm and baffle spacing of 165 mm. The observed back pressure for this configuration was 3833 Pa. This is the least value of back pressure. From the results above, it was observed that the Case-4 muffler model is showing least back pressure than Case-1, Case-2 and Case-3 muffler model.

3.5 CASE-5 SIMULATION:

In this modification the baffle spacing was adjusted to 175 mm and perforation size was 3 mm. The back pressure was 4150 Pa.

3.5 CASE-6 SIMULATION:

In this modification the baffle spacing was adjusted to 175 mm and perforation size was 3 mm. The back pressure was 4020 Pa.
3.6 CASE-7 SIMULATION:
In this modification, pitch size was 4 mm and perforation size was unchanged. The back pressure was 3980 Pa.

![Velocity Distribution](image1)
![Pressure Distribution](image2)

**Fig 3.7 Velocity and Pressure Distribution for Case-7**

<table>
<thead>
<tr>
<th>Sr. No.</th>
<th>Perforation Size</th>
<th>(d/p) Ratio</th>
<th>Baffle Spacing</th>
<th>Back Pressure, Pa (CFD)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
<td>At 20 m/s</td>
</tr>
<tr>
<td>Case 1</td>
<td>3 mm</td>
<td>0.6</td>
<td>180 mm</td>
<td>487</td>
</tr>
<tr>
<td>Case 2</td>
<td>4 mm</td>
<td>0.8</td>
<td>180 mm</td>
<td>444</td>
</tr>
<tr>
<td>Case 3</td>
<td>4 mm</td>
<td>0.8</td>
<td>165 mm</td>
<td>440</td>
</tr>
<tr>
<td>Case 4</td>
<td>3 mm</td>
<td>0.6</td>
<td>165 mm</td>
<td>421</td>
</tr>
<tr>
<td>Case 5</td>
<td>3 mm</td>
<td>0.6</td>
<td>175 mm</td>
<td>-</td>
</tr>
<tr>
<td>Case 6</td>
<td>3 mm</td>
<td>0.6</td>
<td>170 mm</td>
<td>-</td>
</tr>
<tr>
<td>Case 7</td>
<td>3 mm</td>
<td>0.75</td>
<td>180 mm</td>
<td>-</td>
</tr>
</tbody>
</table>

The fig.3.8 shows the graph of comparison of back pressure of all the four muffler cases against flow velocity. It is clearly seen that the modification with baffle spacing of 165 mm produces least back pressure.

**Fig. 3.8 CFD Simulation Results**

**CONCLUSIONS**
1. The configuration with perforation diameter 3 mm and baffle spacing 165 mm creates the least back pressure.
2. The back pressure for the case-4 muffler is 3833 Pa whereas the back pressure for the base model is 4196 Pa. Thus, there is a discrepancy of 3.25% between CFD and experimental results.
3. The Case-3 muffler doesn’t give satisfactory results compared to Case-4. This is due to the fact that though Case-3 combines Case-2 and Case-4, the effect of decrease in number of perforations is more predominant.
4. The Case-7 muffler with 180 mm spacing and d/p ratio 0.75 also gives satisfactory results and it can be considered for validation in future work.

REFERENCES


